

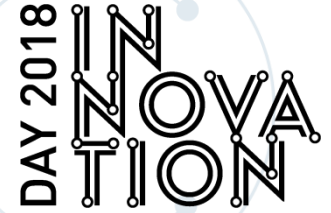
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SESSION 2
Umfeldsensorik mit
LiDAR

»Umfeldererkennung in autonomen mobilen Systemen«

Werner Brockherde, Fraunhofer IMS

Outline

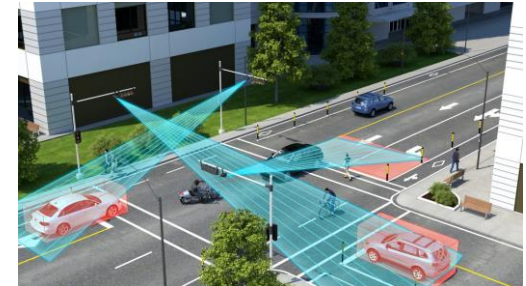


- LiDAR Technology
- Solid-State Photodetectors
- Design example
- Service of FMD

Lidar for automated driving

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- LiDAR/LaDAR = Light/Laser Detection and Ranging
- Range determination by time-of-flight measurement
- To date mostly used in geoscience and military applications with use of active laser illumination in SWIR for eye-safety
- In automotive:
 - Use of active laser illumination, typically in NIR (905 nm)
 - Size, costs, and reliability become most important



©Leddartech

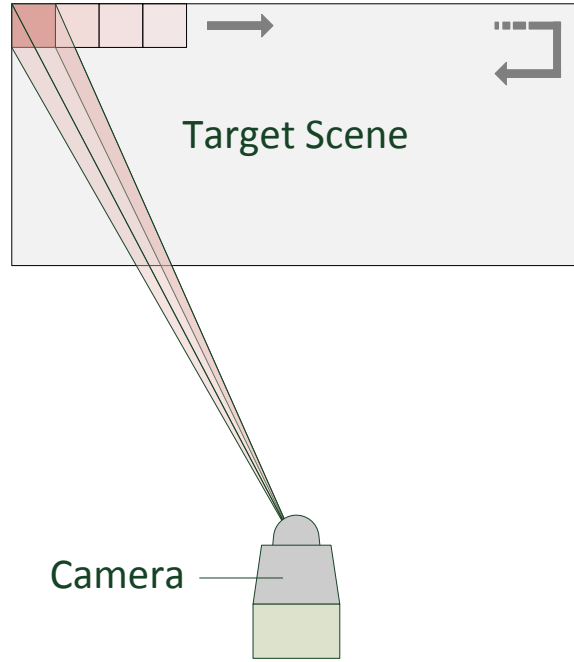
LIDAR-Methods: Scanning lidar

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- Subsequent pointing to object area points
- Mechanical scan
- High optical power density
- High distance range
- Single detector element
- Only one object point at a time
- Low framerate
- Bulky and expensive

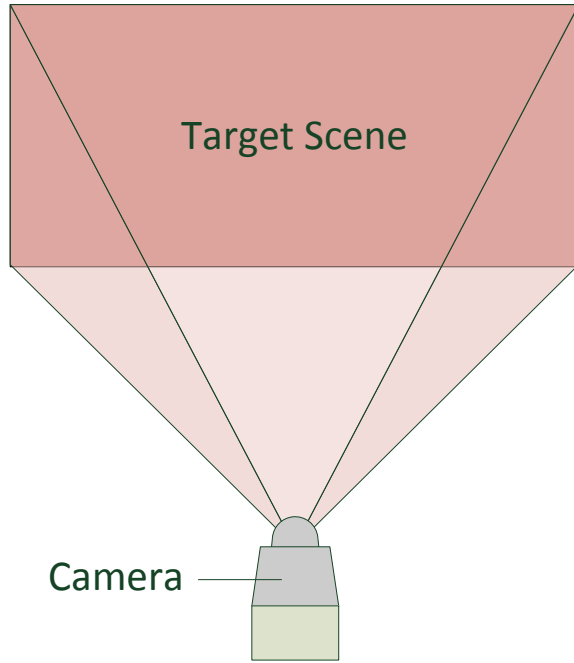


LIDAR-Methods: Beam steering



- Using **Micro Mirrors** or **Optical Phased Arrays**
- Subsequent pointing to object area points
- High optical power density
- Medium/High distance range
- **Detector array required**
- Only one object point at a time
- Low/moderate framerate
- Small size and low cost

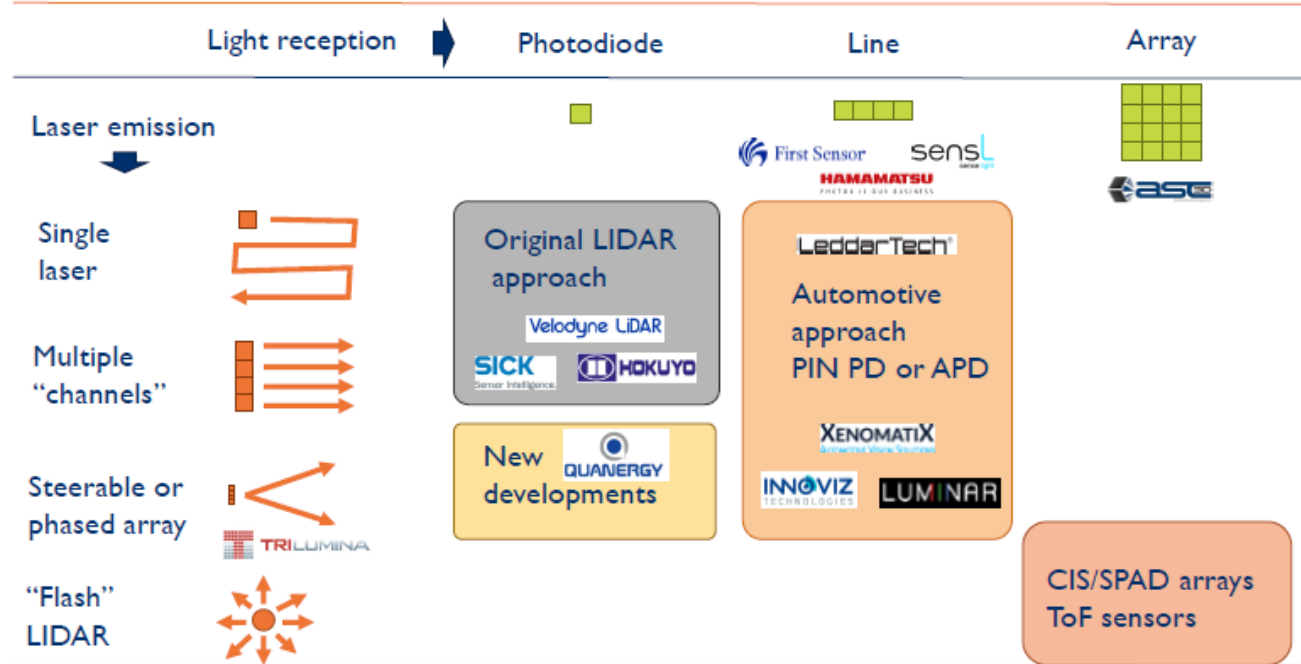
LIDAR-Methods: Flash LiDAR



- Complete scene is taken in a flash
- **Solid state solution possible**
- No moving parts
- Low optical power density
- Low/Medium distance range
- Detector array required
- **High Framerate**
- **Small size and potentially low cost**

LIDAR-Methods

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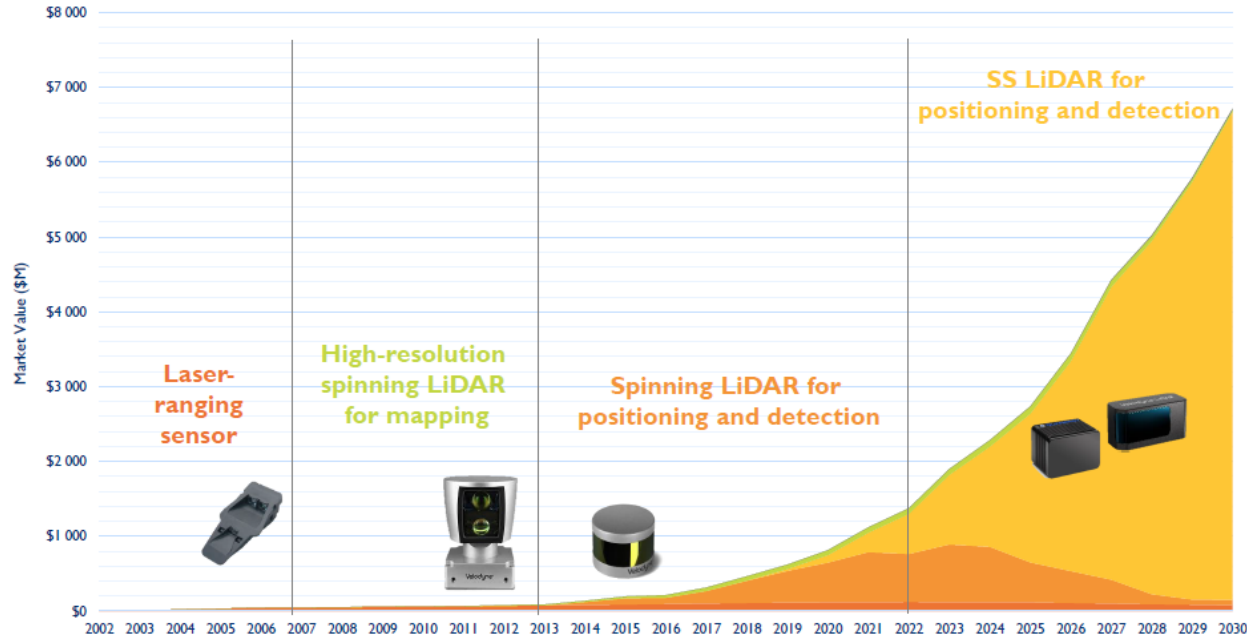
Source:
Yolé 2017



LIDAR-Methods – Market perspective

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Evolution of the LiDAR technology market value in automotive - (\$M)



Source:
Yolé 2017



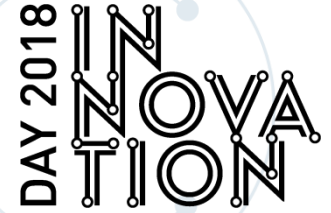
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- LiDAR Technology
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Photodetectors for LiDAR



905 nm

- Silicon detectors
- Compatible to CMOS process technology
- High volume production possible
- Low cost

The 905 nm LiDAR is restricted to lower laser power and hence lower ranges compared to 1500 nm LiDAR

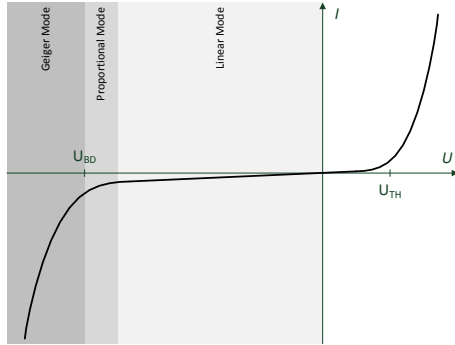
But it is best suited for low-cost systems

1500 nm

- III/V semiconductor detectors
- To be connected to Readout IC
- Performance is temp. dependent
- No high volume production yet

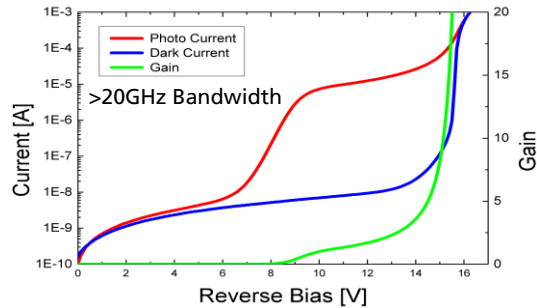
LiDAR @1500 nm allows much more laser power for eye-safe operation and hence is very useful in high-performance applications.

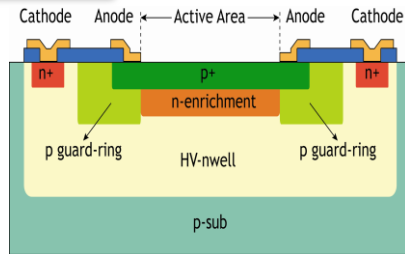
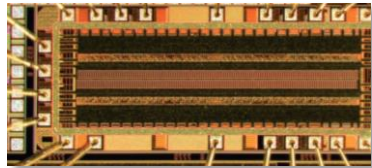
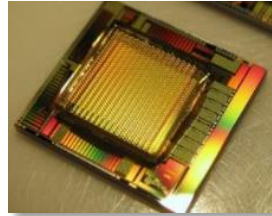
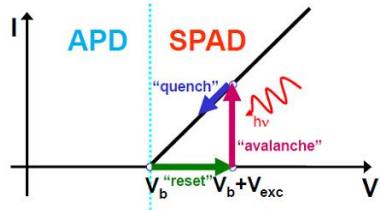
It is also less sensitive to background light



Avalanche photodiodes

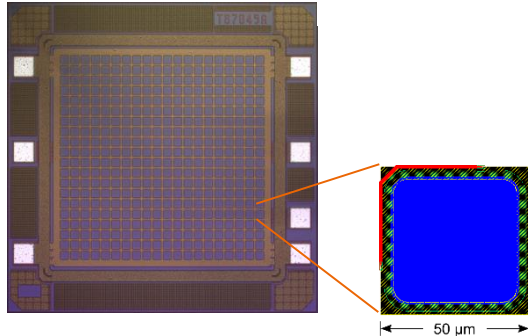
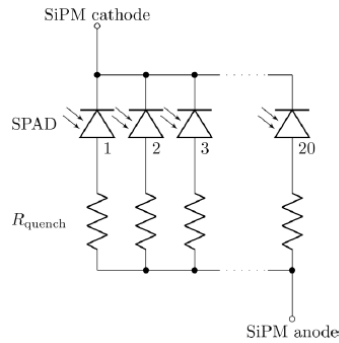
- Operation in proportional mode
- Gain is sensitive to bias and temperature variations
- Small arrays possible
- Available also for SWIR (~1500 nm)





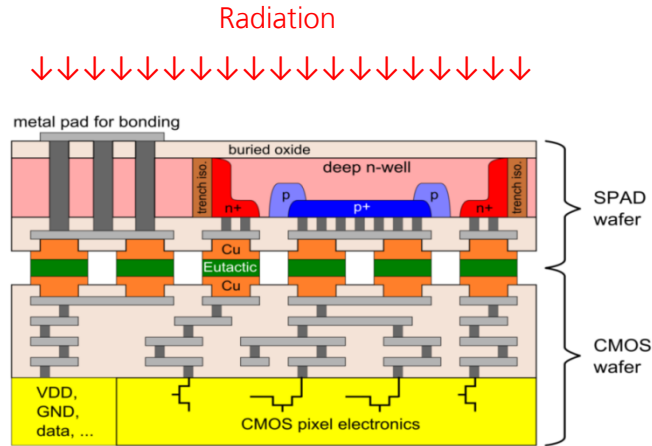
Single-Photon-Avalanche-Diode (SPAD)

- Avalanche photodiode operated above breakdown voltage (= Geiger-Mode)
- Very few photons can be detected
- CMOS integration allows for high spatial resolution and on-chip signal processing
- Fast operation with very good time resolution
- No analog signal processing needed



Silicon Photomultiplier SiPM

- Avalanche photodiodes in Geiger mode
- High gain and single-photon resolution
- CMOS integration allows on-chip pre-amplification and small arrays of SiPMs
- Example:
 - 20×20 SPAD-elements on 1×1 mm² active area
 - Geometric fillfactor: 68% @ 50μm pitch
- SiPMs are also used in high-energy physics or PET

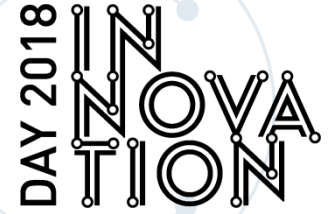


Schematic cross section of backside illuminated SPAD sensor after integration

Backside Illuminated SPAD arrays


- High density CMOS readout circuit
- Optimized Si-wafers for best SPAD performance
- Wafer to wafer bonding process allows for higher production volumes
- Process more complex, but chip size can be drastically smaller

Silicon Photodetectors



	PIN-PD	APD	SiPM	SPAD
Gain	1	10^3	10^6	10^6
Single photon detection	No	No	Yes	Yes
Operational Bias	Low	Medium	Medium	Medium
Temperature Sensitivity	Low	High	Low	Low
Array possible	Limited	Limited	Limited	Yes
Readout / Electronics	Complex	Complex	Medium	Simple (digital)
Rise time	Medium	Slow	Fast	Fast

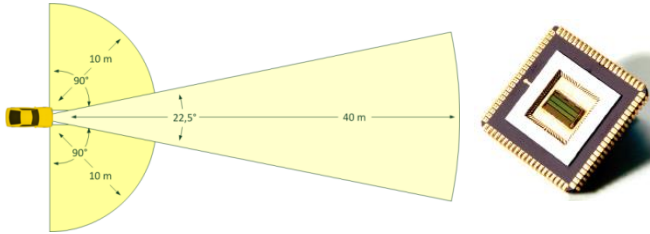
Outline



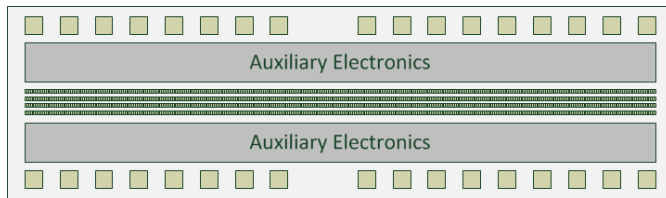
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- LiDAR Technology
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Design proposal for flash LiDAR



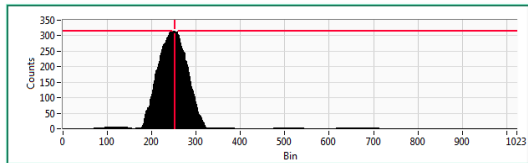
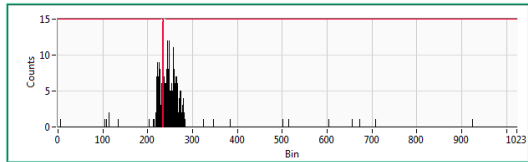
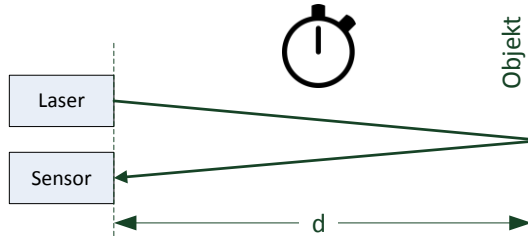
- Detection of target area by 4 lines
- Different FoVs and ranges
- Medium ranges < 100 m
- Detector allows high fillfactor
- Low vertical resolution may be overcome by push-broom effect
- Applications:
 - VRU detection
 - Side traffic
 - Parking assistance



Test vehicle: OWL camera with 192 x 2 line sensor

Distance measurement

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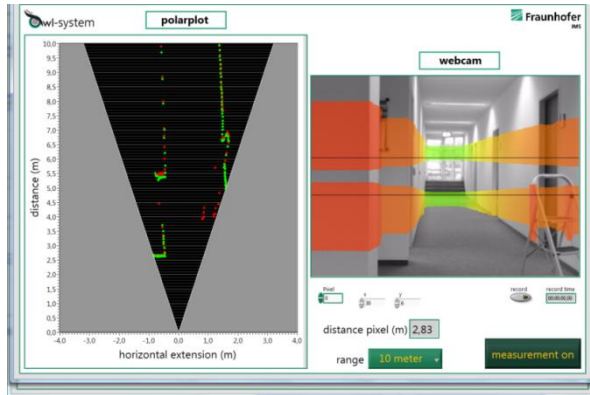
- Laser pulse width: 20ns
- Repetition rate: 10kHz
- 400 pulses per frame
- Evaluation of timing histogram with filters and dedicated algorithms
- TDC resolution ca. 5cm
- Range: > 40 m @ 25fps

Test vehicle: OWL camera with 192 x 2 line sensor

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- 192 x 2 pixel SPAD LiDAR detector
- In-pixel TDCs
- Dynamic Range extension
- Circuitry for background light suppression
- Test with 905nm 75W laser
- FOV (laser): 2x (40,0° x 2,0°)
- Range: > 40 m @ 25fps



Test vehicle: OWL camera with 192 x 2 line sensor

Background light suppression

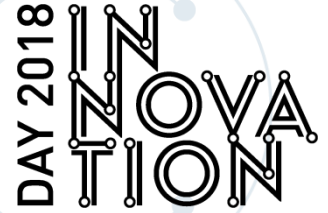
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Video


- Outdoor scene with ca. 90 klx sunlight
- Distance ca. 15 m; 25 fps
- BG light is suppressed

Outline




- LiDAR Technology
- Solid-State Photodetectors
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Service of FMD



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- Concept and feasibility studies
 - Based on existing technologies
 - New approaches, e.g. FMCW-LiDAR
- Modeling of LiDAR Systems in applications including
 - Laser, optics, MEMS, detectors and signal processing
 - Environmental conditions (e.g. sunlight)
- Development of custom photodetectors and photodetector arrays
 - APDs (Si and III/V); SPAD arrays; BSI SPAD arrays; SiPM (-arrays)
- Qualification for series production
- Pilot production



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Thank You !

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SESSION 2 Umfeldsensorik mit LiDAR

»Laserquellen für LiDAR-Systeme«

Dr. Andrea Knigge, Dr. Hans Wenzel
Ferdinand-Braun-Institut
Leibniz-Institut für Höchstfrequenztechnik

Outline

- Diode lasers for automotive LiDAR systems with 905 nm wavelength (FBH)
 - Motivation, Requirements
 - Layer structure, Bragg grating, electronic driver
 - Diode lasers with one and three emitters
- Diode lasers with longer wavelengths (1.5 μm HHI and $> 2 \mu\text{m}$ IAF)
- Summary

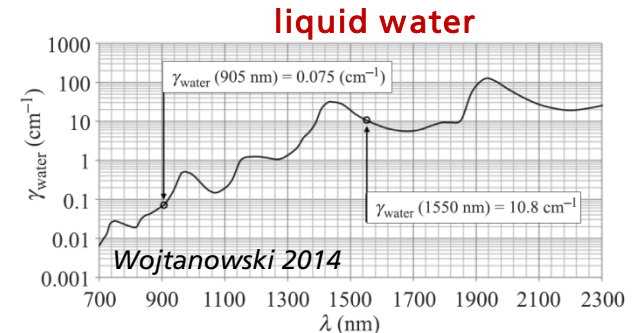
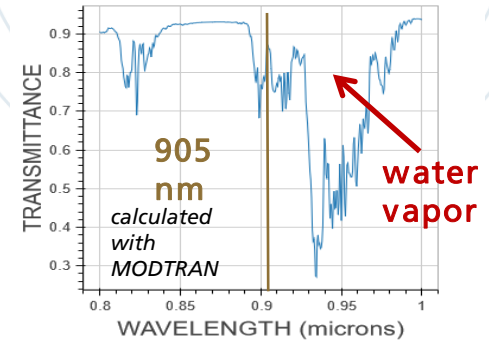


<https://www.bosch-presse.de/pressportal/de/de/neue-sensorik-fuer-intelligente-automatisierung-78080.html>

Requirements for lasers to be used for automotive point-scanning time of flight (TOF) LiDAR

- Application under real atmospheric conditions
 - ⇒ emission wavelength within transparency window ⇒ $\lambda = 905 \text{ nm}$
 - ⇒ wide working temperature range (-40°C ... +85°C) to enable non-temperature stabilized operation
 - ⇒ suppression of sun light to improve SNR ⇒ emission within a small spectral window < 10 nm over whole temperature range
 - ⇒ wavelength stabilization by monolithic integrated Bragg grating
 - ⇒ adapted layer structure
- High temporal resolution and eye safety
 - ⇒ short pulses < 10 ns ⇒ layer structure optimized for high current densities
- Large scanning range
 - ⇒ pulse power of 100 Watt ⇒ broad-area edge-emitting laser diode
- High spatial resolution
 - ⇒ sufficiently good beam quality ⇒ optimized emission aperture

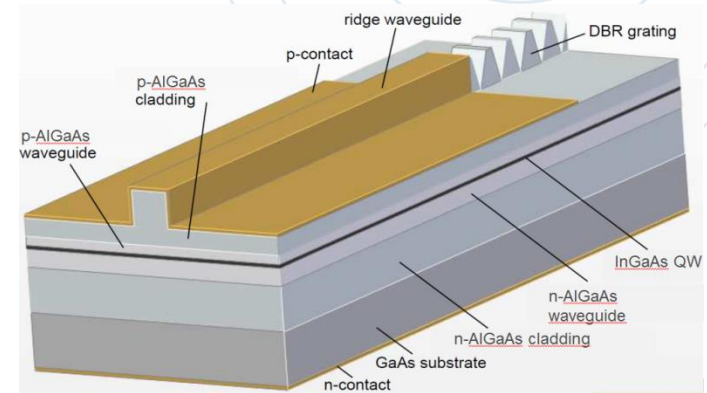
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FBH device: Distributed Bragg reflector (DBR) broad area (BA) laser

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- GaAs-based
- single-step MOVPE
- emission wavelength near 905 nm at RT
- lateral optical and electrical confinement by dry-etched trenches
- contact widths: $W = 30, 50, \text{ or } 100 \mu\text{m}$
- total cavity length $L = 6 \text{ mm}$
- higher-order surface Bragg grating integrated in the rear part of the cavity, $L(\text{DBR}) = 1 \text{ mm}$
- suitable for p-up or p-down mounting



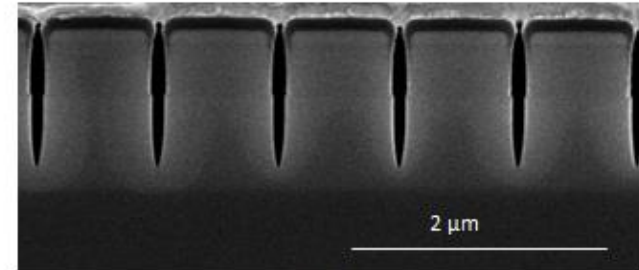
Structure for pulsed automotive LiDAR application controlled by simulation using drift-diffusion based model (VIAS-TeSCA):

- only small carrier accumulation at high current densities (strongly reduced leakage currents and additional free carrier absorption)

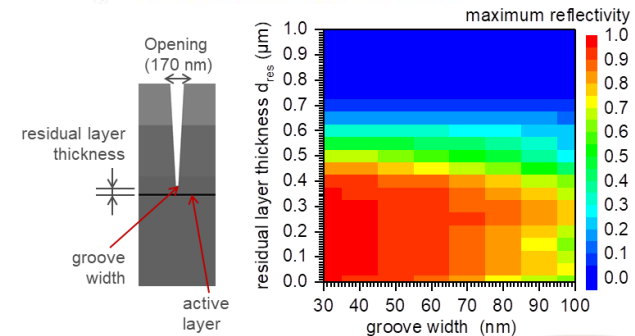
Design of surface Bragg grating

- Processing
 - E-beam lithography (i-line wafer stepper alternative)
 - dry-etching
 - no regrowth (single step MOVPE)
- Parameters
 - 7th order, period 960 nm
 - length of grating LDBR = 1 mm
 - opening of V-shaped slits 170 nm
 - width at bottom (groove width) and residual layer thickness
- Simulation of grating reflectivity with mode matching tool
 - peak reflectivity > 90% for residual layer thickness up to 0.3 μm and groove widths < 50 nm
 - absorption losses neglected

Fricke 2012



SEM picture of cleaved DBR section



GaN Pulse Laser Drivers for LiDAR

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■ Specs

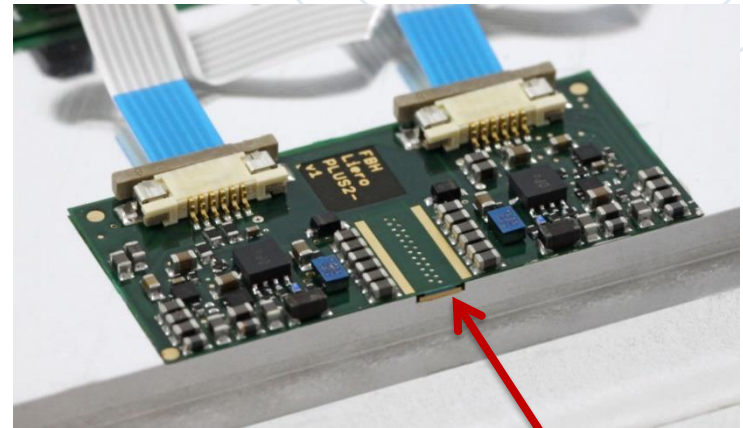
- Lasers with > 100 W peak power
- Pulse widths 3 ... 10 ns
- Switching currents > 100 A_{pp}

■ Challenges

- Transistors with high-speed high-current capabilities
- Low-inductive assembly

■ Solution

- GaN offers best performance
- Hybrid circuit with CMOS & GaN
- TTL input
- Dedicated mounting scheme



laser

Single emitter diode laser: Pulse characteristics

- Known or measured quantities
 - repetition frequency f
 - average current I_{av} and power P_{av}
 - lateral near field intensity $NF(x,t)$ versus time
- Derived quantities

pulse energy $E = \frac{P_{av}}{f} = 130 \text{ nJ}$

pulse shape $p(t) = \int NF(x,t) dx$

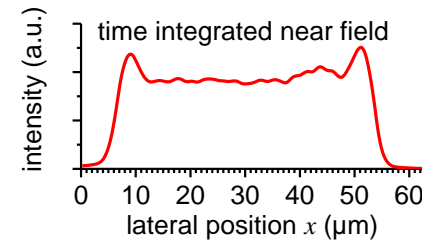
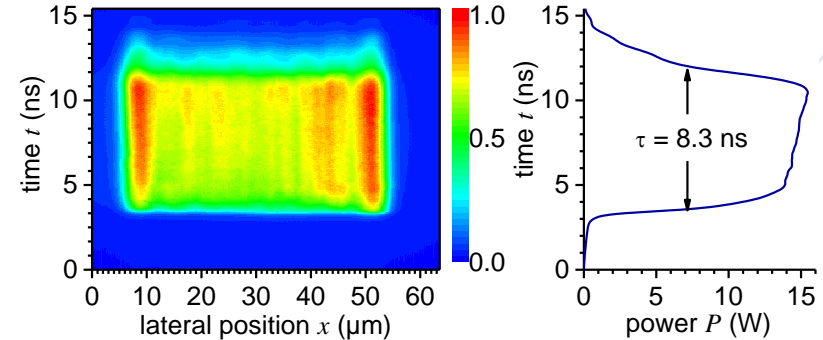
power vs. time $P(t) = \frac{p(t)E}{\int p dt}$

pulse width $\tau = \text{FWHM of } P(t) = 8.3 \text{ ns}$

pulse power $P_{pulse} = \frac{E}{\tau} = 15.7 \text{ W}$

current $I = \frac{I_{av}}{\tau f} = 20.5 \text{ A}$

time resolved lateral near field intensity $NF(x,t)$
streak camera (100 pulses averaged)



$\tau_{Gen} = 10 \text{ ns}$
 $f = 10 \text{ kHz}$
 $I_{av} = 1.7 \text{ mA}$
 $P_{av} = 1.3 \text{ mW}$

Klehr 2018

Single emitter diode laser: Power and optical spectra in dependence on temperature

■ Pulse power P

- up to 33 W @ T = 25°C
- up to 28 W @ T = 85°C

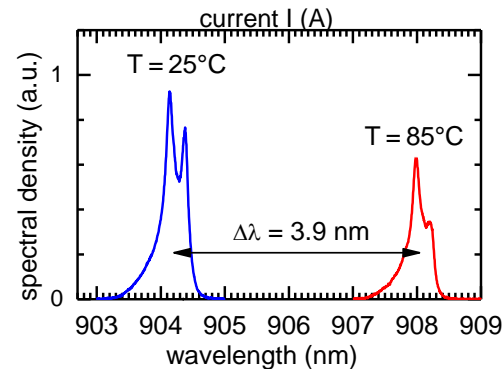
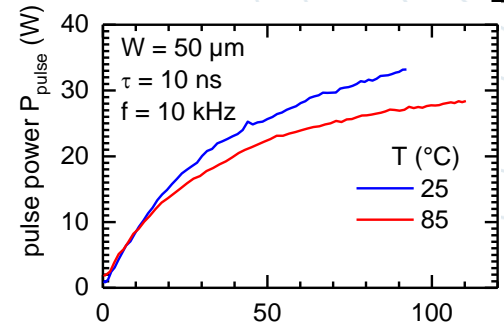
starting saturation for P > 15 W or I > 20 A

■ Time-averaged optical spectra

- spectral shift $\Delta\lambda = 3.9$ nm for $\Delta T = 60$ K
 $\Rightarrow \Delta\lambda / \Delta T = 65$ pm/K
 $\Rightarrow \Delta\lambda \sim 8$ nm for T = [-40°C, +85°C]
(would be $\Delta\lambda \sim 40$ nm without Bragg

grating)

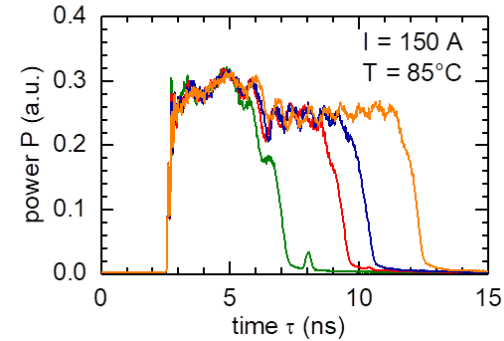
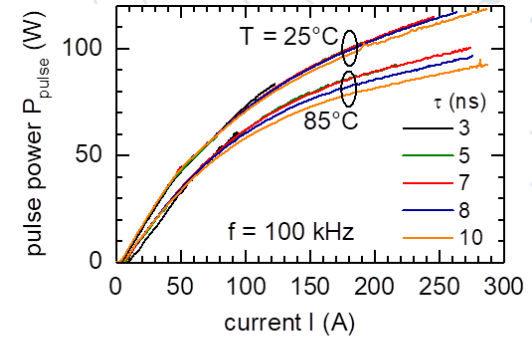
- spectral width: < 0.5 nm



A. Knigge 2018

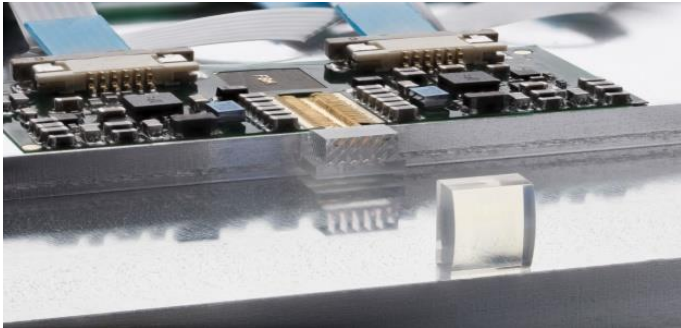
3-emitter diode laser: Power and optical spectra in dependence on temperature

- 3-emitter chip:
 - adjustable optical pulse length: 3 ns ... 10 ns
 - maximum optical pulse power:
 - $P_{\text{pulse}} = 120 \text{ W} @ T = 25^\circ\text{C}$
 - $P_{\text{pulse}} = 100 \text{ W} @ T = 85^\circ\text{C}$
- Pulse shape
 - steep pulse edges
 - \Rightarrow good matching of electrical driver and laser chip with minimized distances for low inductive losses

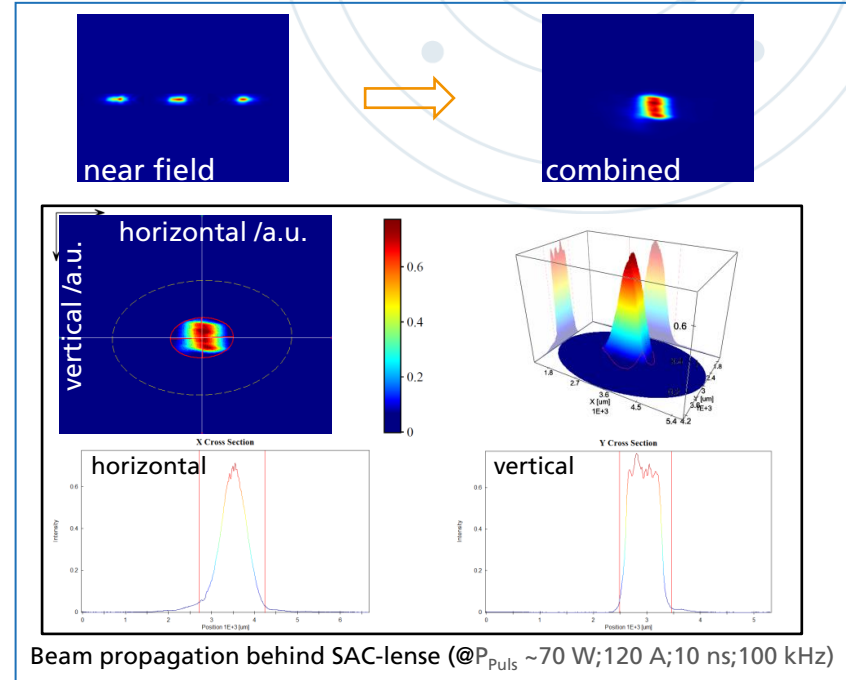


Beam collimation of 3-emitter chip

- 3 emitters combined with fast and slow axis collimation and BeamTwister™ by FISBA Photonics GmbH, Berlin
- Remaining divergence: 5 mrad (H) / 3 mrad (V)
- 90 cm x 56 cm spot after 180 m (calculated)



FISBA



Flexible technology kit for a broad range of LiDAR applications

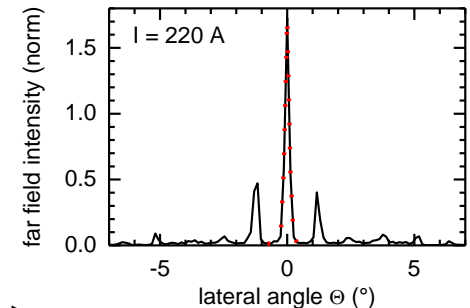
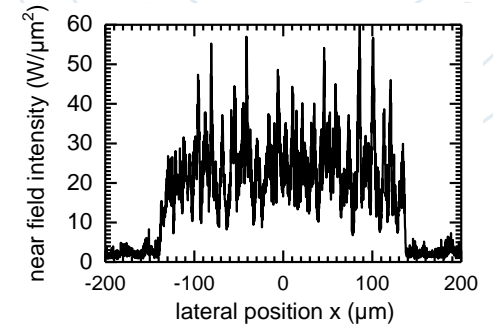
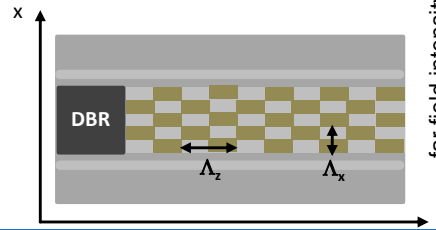
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- In a single housing:
 - laser chip directly integrated with driver unit
 - electrical and programming control unit
- At present on hand:
 - wavelength: 905 nm, wavelength-stabilized
 - optical pulses: 0,4 – 20 ns
 - optical pulse power up to 100 W
 - switching currents up to 250 A
 - internal or external trigger
 - repetition frequency 10 kHz – 1 MHz
- Other configurations on request



Next steps of development of 905 nm diode laser

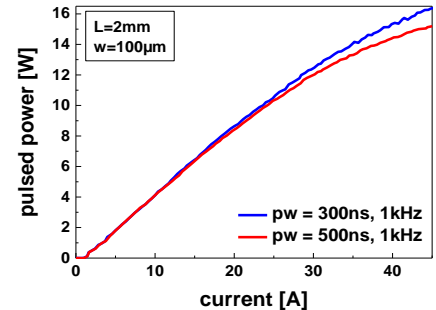
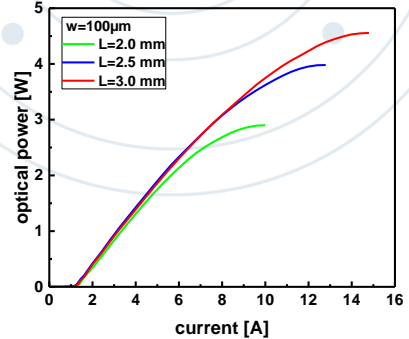
- Further power increase:
 - Increase of emitter width \Rightarrow decrease of beam quality
 - Bars with up to 48 DBR emitters
- Improvement of lateral beam quality (smaller spot size)
 - periodic lateral (x) and longitudinal (z) gain and index variations
 - results of a simulation with WIAS-BALaser:
 - total power $P = 80$ W
 - central lobe:
 - $P_{cl} = 32$ W
 - $Q_{95\%,cl} = 0.65^\circ$, $W_{95\%} = 272$ μm
 - $BPP_{95\%,cl} = 0.77$ mm mrad, $B_{95\%,cl} = 41$ W/(mm mrad)



Fraunhofer-Institut für Nachrichtentechnik, Heinrich-Hertz-Institut, HHI: InP diode lasers for $\sim 1.5 \mu\text{m}$

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- Advantages compared to 905 nm:
 - lower solar radiation background
 - better performance under hazy conditions (lesser scattering loss)
 - much higher eye safety power limit
- Available InP diode lasers at $1.5 \mu\text{m}$ from HHI:
 - BA-lasers: cw operation: 5 W; pulsed operation: 16 W (300 ns), thermally limited \rightarrow much higher output power possible at 5 ns for pulsed LiDAR
 - coherent light source; tunable lasers for beam steering for FMCW LiDAR
- Special adaption for LiDAR systems possible also with detector integration



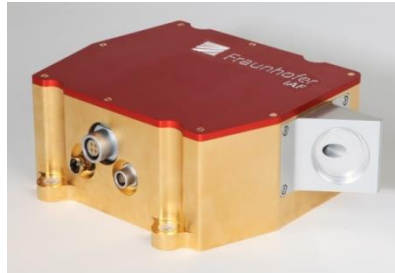
Fraunhofer-Institut für Angewandte Festkörperphysik, IAF: Semiconductor lasers for 2 – 11 μm wavelength range

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- In comparison to 905 nm:
 - Higher visibility range due to lower scattering losses
 - Eye safety: lower Nominal Ocular Hazard Distance, i.e. higher power permitted
- Applications:
 - Military: Long-range surveillance and reconnaissance
 - Security: Support of task forces and rescue teams under degraded visual environments
 - Space: Atmospheric research and earth observation

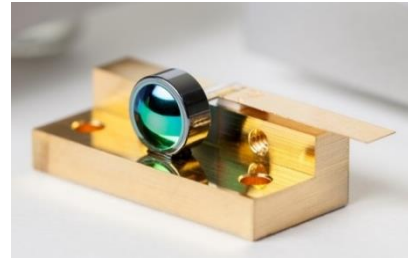
Semiconductor Disk Lasers (SDLs) for 2 – 3 μm :

- Output power > 1 W at 25°C
- Spectral line width > 20 kHz (stabilized)
- Pulse length > 32 ns
- Pulse energy < 3.3 mJ

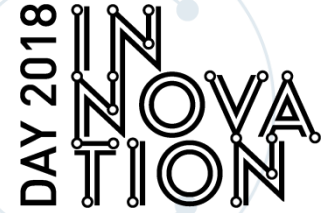


Quantum Cascade Lasers (QCLs) for 4 – 11 μm :

- Output power > 0.5 W
- Spectral tuning range < 300 cm^{-1}



Summary



- Distributed-Bragg-reflector broad-area laser integrated in a nanosecond electronic driver suitable of automotive LiDAR
 - optical pulse lengths 3 ... 10 ns
 - emission wavelength 904 nm @ T = 25°C
 - wavelength shift < 10 nm between temperatures of -40°C and +85°C
 - pulse power 100 W @ 85°C (3-emitter chip)
 - spot of combined beam 90 cm x 56 cm at distance of 180 m
 - ease of manufacture due to higher-order surface grating
 - flexible technology kit available: single housing for diode laser, electrical and programming control unit
- 1.5 μm wavelegth: BA diode lasers available, adaption for LiDAR application possible
- 2 – 11 μm wavelength range: Semiconductor Disk Lasers and Quantum Cascade Lasers available

With thanks to:

- Ferdinand-Braun-Institut:
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- Fraunhofer-Institut für Angewandte Festkörperphysik, IAF:
 - Ralf Ostendorf
 - EU project »MIRPHAB« – Mid-infrared photonics devices fabrication for chemical sensing and spectroscopy applications
 - Research contracts with German MoD (BMVg, WTD91)

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SESSION 2 Umfeldsensorik mit LiDAR

»Mikrospiegel für die Laserstrahlführung«

Jörg Amelung, FMD

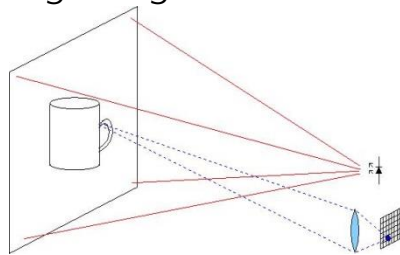
Time of Flight (ToF) 3D-Distance Measurement

Parallel Data Capture 3D-Cameras



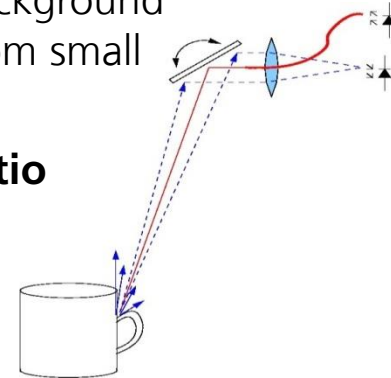
Serial Data Capture Laser Scanners

- Signal light is distributed over entire FOV of 3D measurement (small intensity per Pixel)
- collects Signal- und background light over long integration times

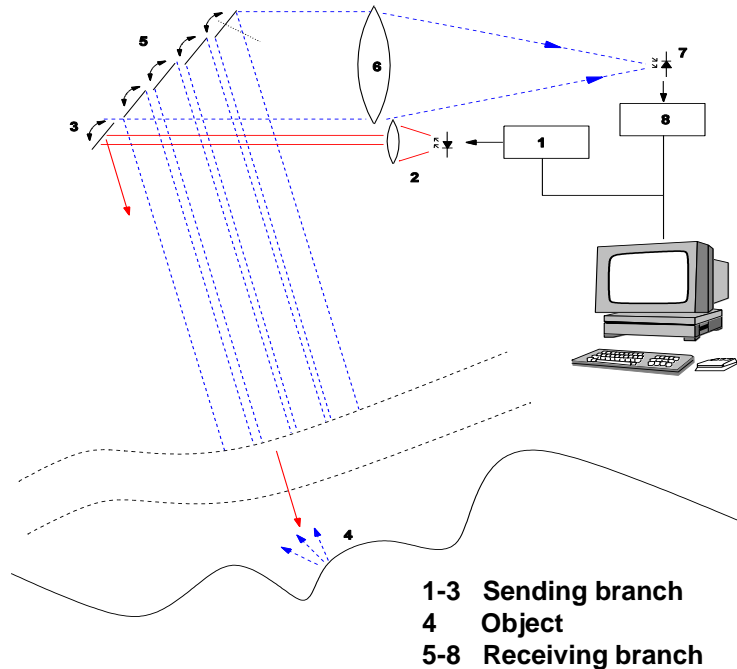


- Single measuring points are illuminated sequentially within FOV
- collects light of signal- & background (noise) in short time only from small measured area

⇒ **Enhanced signal/noise ratio**



MEMS based LIDAR Scanner Concept



Distance Laser Scanner using MEMS

Advantages

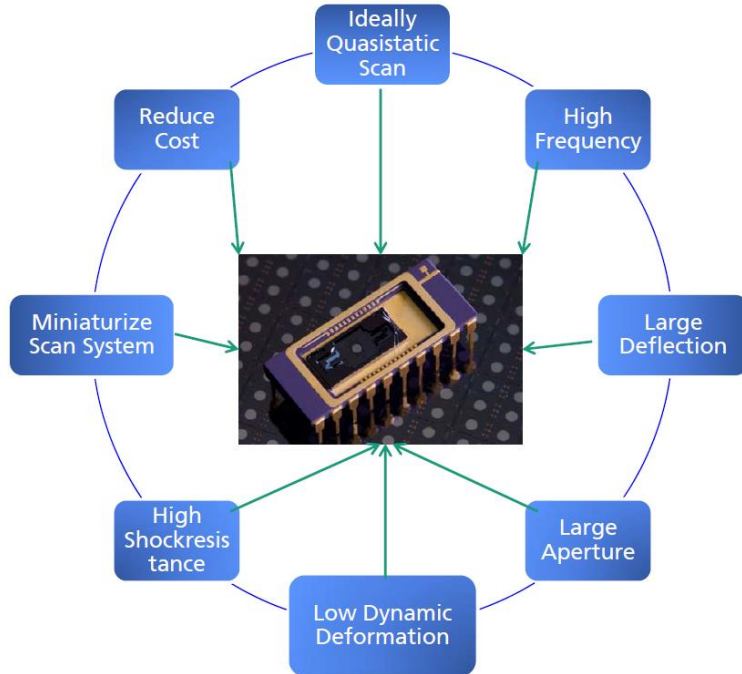
- + **fast scanning** (no air bearings)
- + **low weight, very robust**
- + (potentially) low cost

Challenges

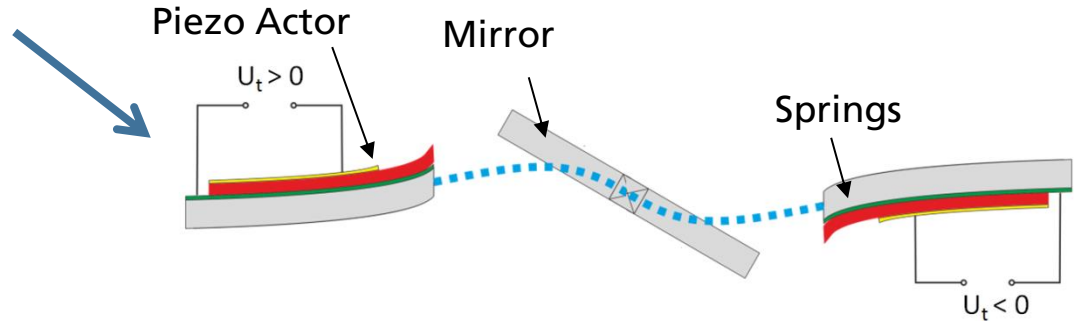
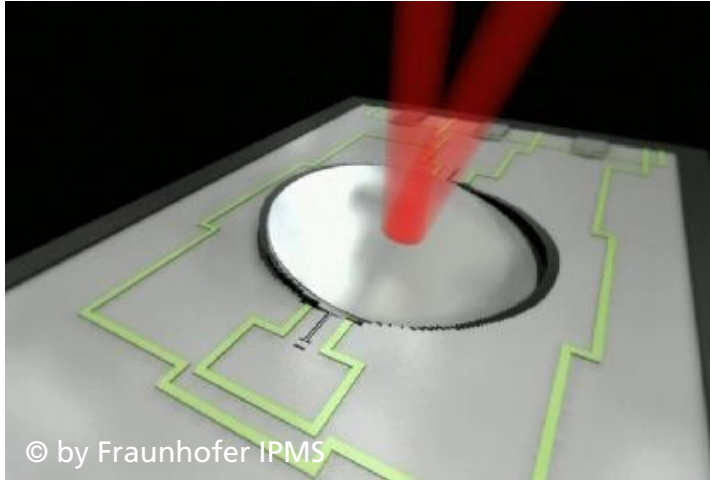
- **large receiving aperture indispensable**
⇒ **several mirrors required** in reception branch to enable **large amplitude**
- ⇒ **synchronized movement of all mirrors**

MEMS Mirror requirements for LIDAR applications

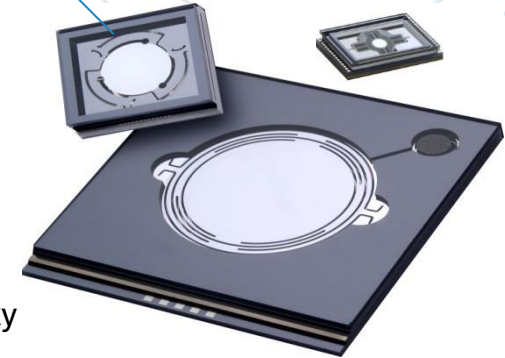
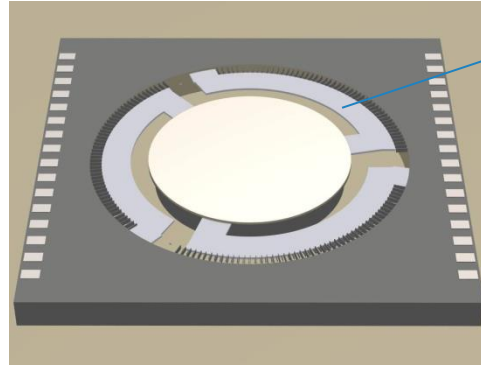
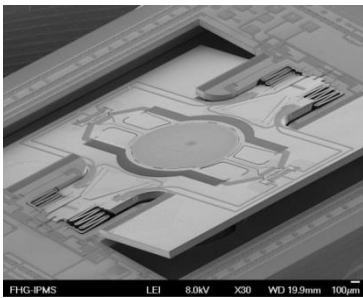
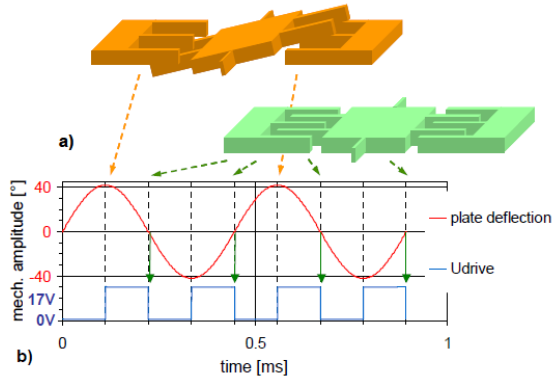
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MEMS Mirror Principles



Resonant principle for combdrive

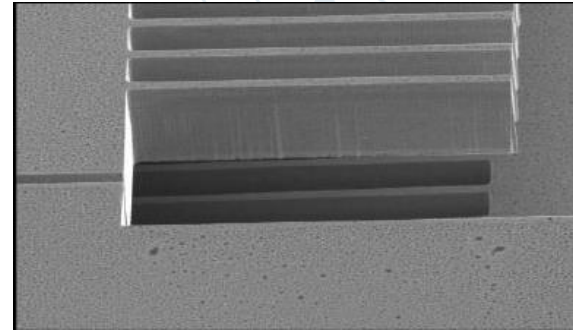
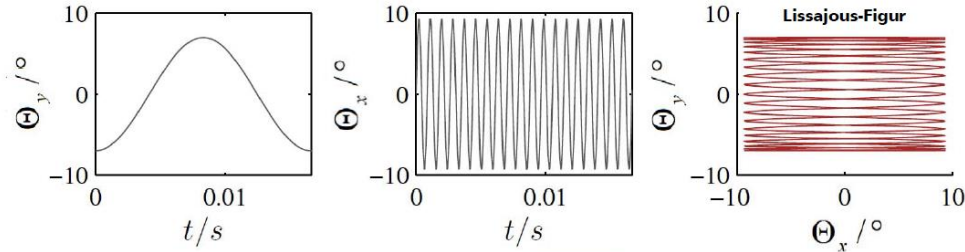


- Identical resonant frequencies in xy
- Minimum chip-size
- Circular springs enable large tilt angle
- Advantageous eigenmode spectrum

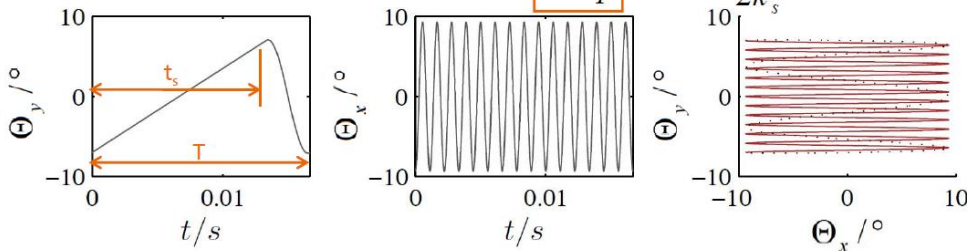
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Resonant and quasistatic-resonant principle for combdrive

Sinus-Sinus (doubleresonant)

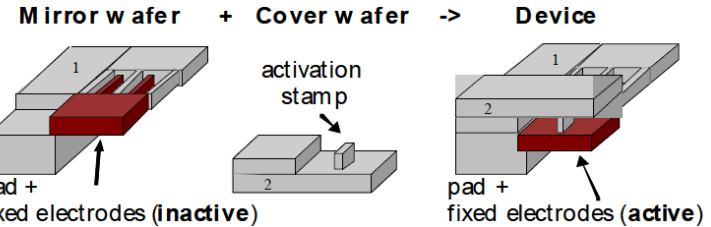


Sawtooth-Sinus (quasistatic-resonant)



$$k_s = \frac{t_s}{T}$$

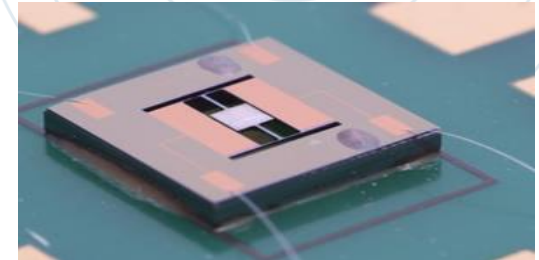
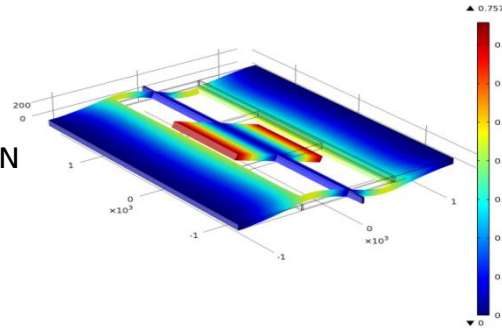
$$f_{xq} = \frac{1}{2k_s} N_y f_y$$



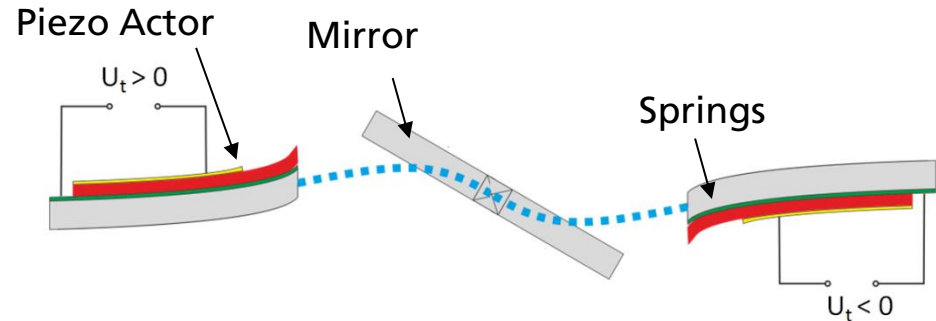
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Piezoelectric actor principle

- **Unimorph MEMS structures**
 active layer: AlN, PZT, AlScN
 typical electrodes: Pt, Mo, Ti, Cr/Au
 typical passive layer: mono-Si, poly-Si, SiO₂, AlN
- **AlN**
 non-ferroelectric, IC-compatible
 low loss dielectrics, bipolar
 $e_{31,f} \approx 1.08 \text{ C/m}^2 \rightarrow$ sensor material
- **Al_{0.57}Sc_{0.43}N**
 non-ferroelectric, IC-compatible
 low loss dielectrics, bipolar
 $e_{31,f} \approx 3.16 \text{ C/m}^2 \rightarrow$ sensor/actuator material
- **PZT**
 ferroelectric, non IC-compatible
 lead zirconate titanate, Pb(Zr_xTi_{1-x})O₃, x ≈ 52%
 $e_{31,f} \approx 21 \text{ C/m}^2 \rightarrow$ actuator material



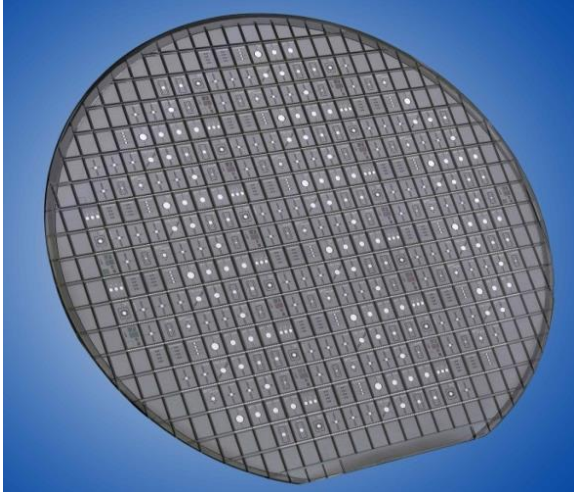
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Integration Issue

Hermetic Wafer Level Vacuum Packaged MEMS Mirrors

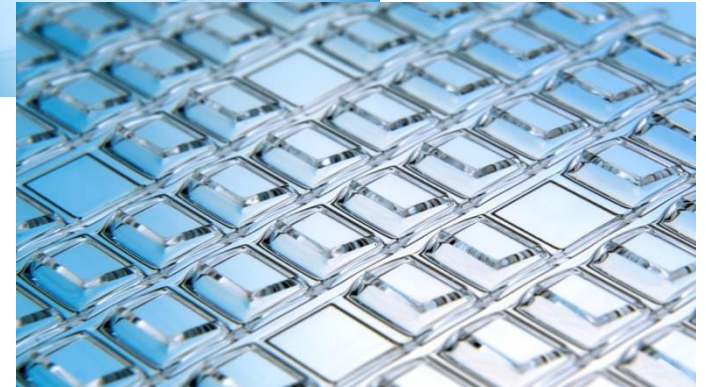
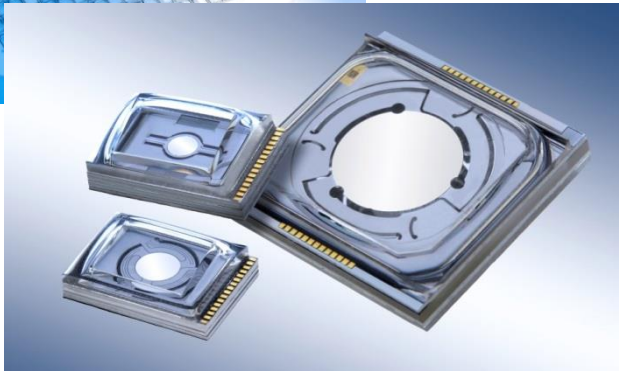
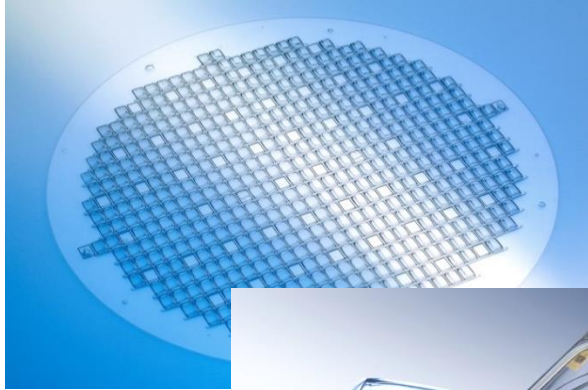
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Unique Glass Forming Technology for WL-Opto-Packages

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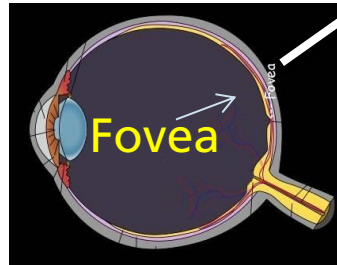
3D-Camera with Object Detection and Foveation

Problem:

- 3D-TOF Sensors are bandwidth limited (max. 1M Voxel/s).

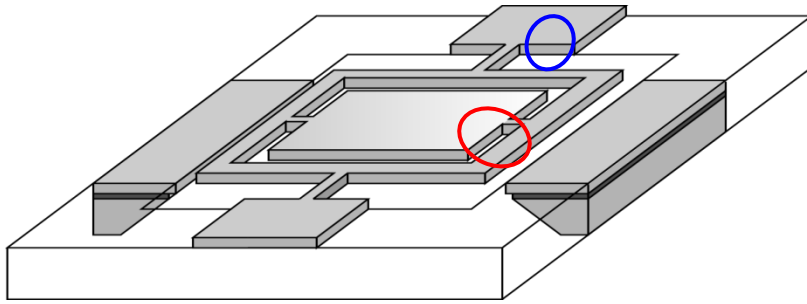
Concept:

- Adaptive 3D-TOF camera with Foveation in analogy to eye
- 2D-MEMS-scanner for fast adaptive scanning required

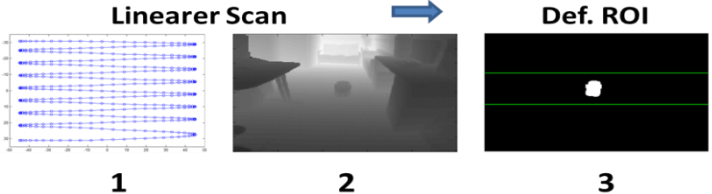


Adaptive 2D Microscanner

Frame
quasistatic

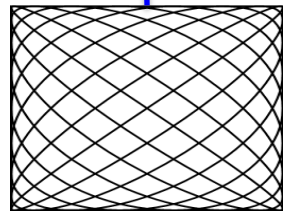
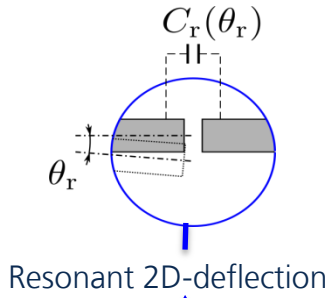


3D data rate is limited to 1 MVoxel / s



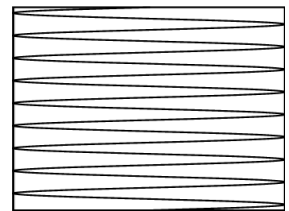
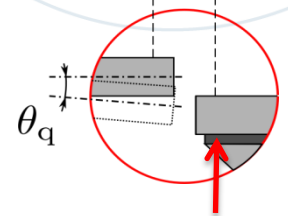
Foveation: resolution locally enhanced within ROI

Inner mirror
resonant



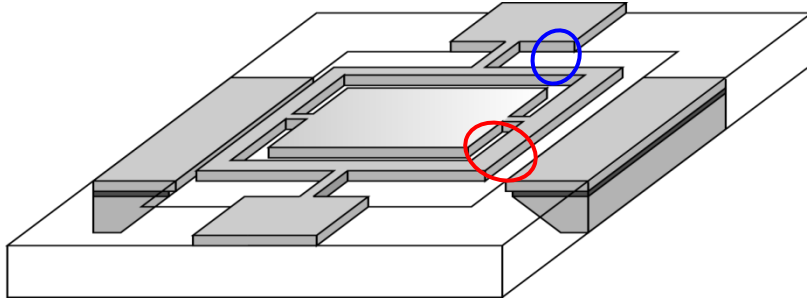
Lissajous-Scan

$C_q(\theta_q)$

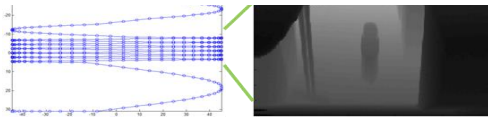


Raster-Scan

Adaptive 2D Microscanner



3D-mapping zoomed within ROI



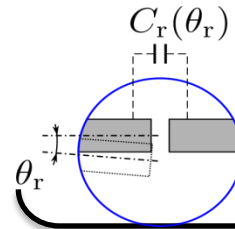
4

5

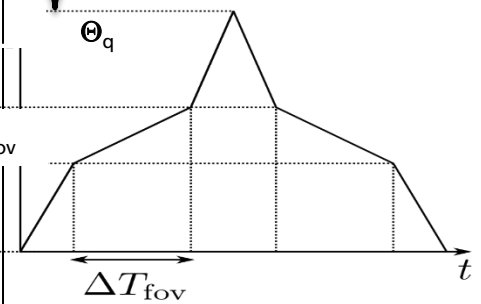
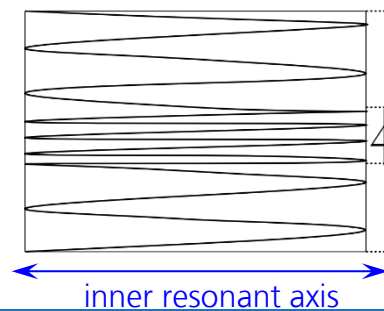
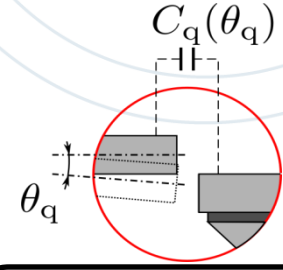
Foveation: continuous intuitive optimised trade-off of resolution and frame rate

Adaptive vertical scan
by
quasistatic frame

Inner mirror resonant

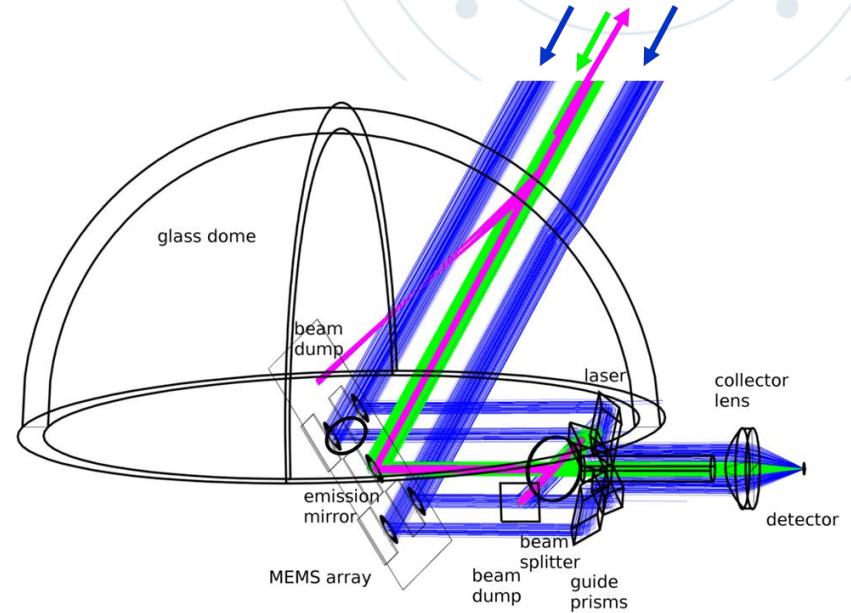
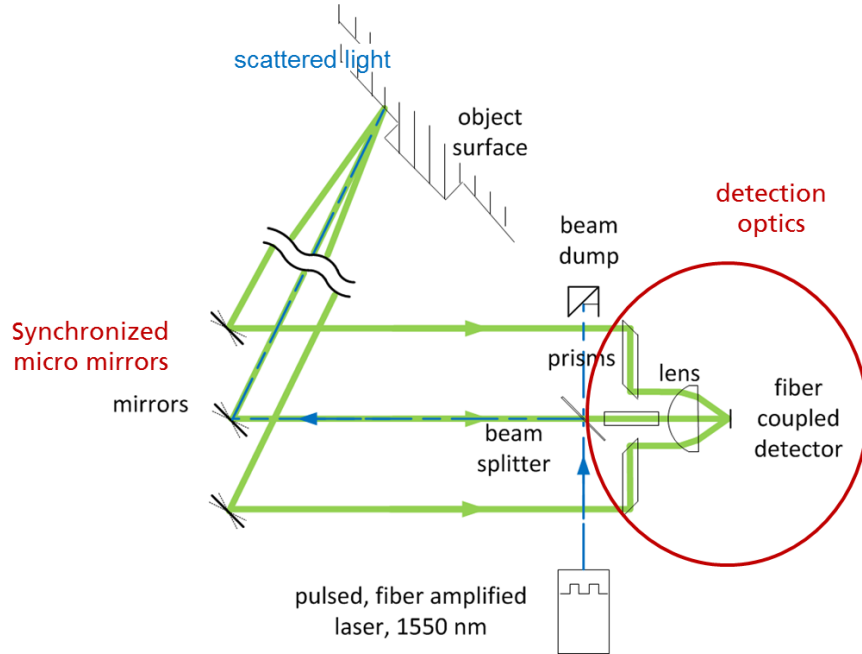


Frame quasistatic



Optical Concept of 3D Camera

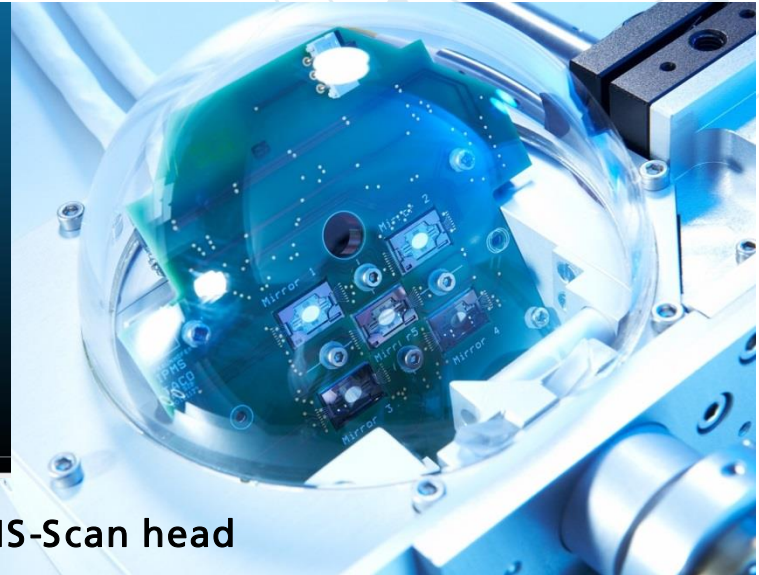
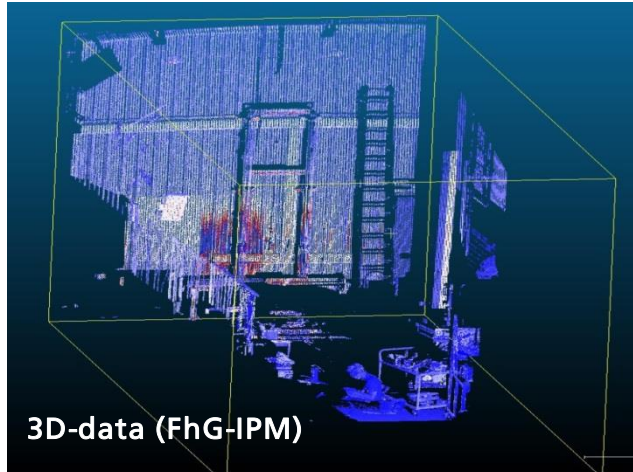
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Adaptive 3D-Laser Camera TACO

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Capability	
Measurement principle	Single-pixel TOF
Field-of-view (max)	80x60 → 60x40
Resolution (max)	250x20 => 1600x1100
Frame rate (max)	240 => 0.5



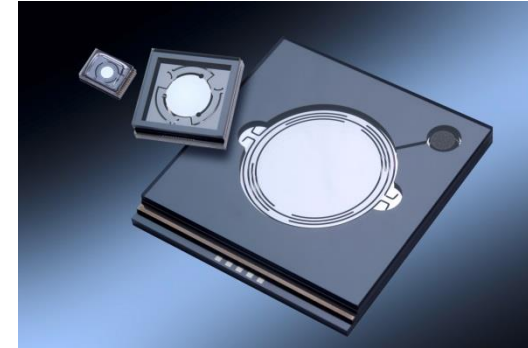
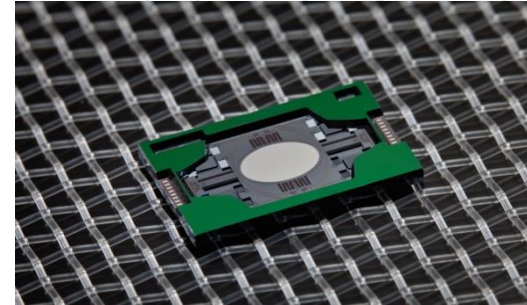
TACO[®]



SEVENTH FRAMEWORK PROGRAMME

Zusammenfassung

- Mikroscooperspiegel, realisiert in Bulk-Mikromechanik, ermöglichen die resonante und quasiresonante Ablenkung von Licht für LiDAR Anwendungen
- Durch die Verwendung von optimierten Scanner-
spiegeln und Scannerspiegelarrays lassen sich
effektive und hochauflösende LiDAR Systeme
realisieren
- Die Institute der FMD haben langjährige Erfahrung
in der Realisierung und Herstellung von Scanner-
spiegel und LiDAR Konzepten



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SESSION 2
Umfeldsensorik mit
LiDAR